# Technical Reference on Hydrogen Compatibility of Materials

High-Alloy Ferritic Steels: Martensitic Stainless Steels Heat Treatable (Fe-Cr type) (code 1820)

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High-Alloy Ferritic Steels:

Martensitic Stainless Steels

Heat Treatable (Fe-Cr type) (code 1820)

#### 1. General

The martensitic stainless steels with low nickel are hardenable by heat treatment to a range of mechanical properties. These alloys are used for their combination of high strength and corrosion resistance [1]. The heat treatment process used to attain high strength in the Fe-Cr type stainless steels involves quenching and tempering.

In general, very little data exists for these alloys in gaseous hydrogen; however, the available data indicate that martensitic stainless steels are susceptible to hydrogen-assisted fracture in gaseous hydrogen, a characteristic common to high-strength alloys. The data from notched tensile tests indicate that this class of alloys is extremely susceptible to fracture in hydrogen environments. Indeed, the Fe-Cr martensitic stainless steels are among the families of alloys that are most susceptible to hydrogen-assisted fracture. Based on the available data, these alloys must be used with caution as structural materials in hydrogen gas service.

### 1.1 Composition and microstructure

The Fe-Cr martensitic stainless steels are distinguished from the precipitation-hardening, martensitic stainless steels by the lack of nickel as an alloying constituent. The Fe-Cr martensitic stainless steels fall into two categories: low carbon and high carbon. Table 1.1.1 lists the approximate composition specification ranges for several common Fe-Cr martensitic stainless steels. Table 1.1.2 provides the compositions of several heats of martensitic stainless steels used to study the effects of hydrogen on mechanical properties.

#### 1.2 Common designations

The Fe-Cr martensitic stainless steels are typically referred to by their AISI designation: type 400-series alloys. The 400-series also consist of a number of non-hardenable varieties, commonly referred to as the ferritic stainless steels (which are not included in this section). There are also a group of similar alloys developed specifically for fusion reactor applications, such as MANET; these are not included.

#### 2. Permeability, Diffusivity and Solubility

We are unaware of any permeation measurements for this class of materials exposed to gaseous hydrogen. Based on electrochemical measurements of effective diffusivity in the precipitation-hardening, martensitic stainless steels, we might expect hydrogren diffusivity to be intermediate between low-alloy steels and austenitic stainless steels: on the order of 10<sup>-12</sup> m<sup>2</sup>/s.

### 3. Mechanical Properties: Effects of Gaseous Hydrogen

## 3.1 Tensile properties

### **3.1.1** Smooth tensile properties

The data in Table 3.1.1.1 show that the ductility of type 410 and type 440C alloys is significantly degraded when tested in high-pressure hydrogen. Hydrogen-precharged type 440C in a low-strength condition also experiences reduced elongation at both room temperature and low temperature (200 K) [2].

### 3.1.2 Notched tensile properties

The data in Table 3.1.2.1 show that the notched tensile strength of type 410 and type 440C martensitic stainless steels is extremely degraded when tested in high-pressure hydrogen. It has also been shown that partial pressures of hydrogen less than an atmosphere can significantly reduce the notched tensile strength of type 410 [3].

#### 3.2 Fracture mechanics

No known published data in hydrogen gas.

### 3.3 Fatigue

No known published data in hydrogen gas.

### 3.4 Creep

No known published data in hydrogen gas.

#### 3.5 Impact

No known published data in hydrogen gas.

### 3.6 Disk rupture testing

Disk rupture tests show that type 410 stainless steel is extremely sensitive to fracture in hydrogen gas [4].

#### 4. Fabrication

The Fe-Cr martensitic stainless steels are available in a range of product forms and a variety of compositions; however, the limited evidence suggests that 400-series alloys are generally susceptible to hydrogen-assisted fracture.

#### 5. References

- 1. RA Lula. Stainless Steel (revised from "An Introduction to Stainless Steel" by JG Parr and A Hanson). Metals Park OH: American Society for Metals (1986).
- 2. GR Caskey. Hydrogen Compatibility Handbook for Stainless Steels (DP-1643). EI du Pont Nemours, Savannah River Laboratory, Aiken SC (June 1983).

- 3. RJ Walter and WT Chandler. Effects of High-Pressure Hydrogen on Metals at Ambient Temperature: Final Report. Rocketdyne (report no. R-7780-1) for the National Aeronautics and Space Administration, Canoga Park CA (February 1969).
- 4. J-P Fidelle, R Bernardi, R Broudeur, C Roux and M Rapin. Disk Pressure Testing of Hydrogen Environment Embrittlement. in: Hydrogen Embrittlement Testing, ASTM STP 543, American Society for Testing and Materials. (1974) p. 221-253.
- 5. ASTM DS-56H, Metals and Alloys in the UNIFIED NUMBERING SYSTEM (SAE HS-1086 OCT01). American Society for Testing and Materials (Society of Automotive Engineers) (2001).
- 6. RP Jewitt, RJ Walter, WT Chandler and RP Frohmberg. Hydrogen Environment Embrittlement of Metals. Rocketdyne for the National Aeronautics and Space Administration, Canoga Park CA (March 1973).

Table 1.1.1. Compositions (wt%) of several Fe-Cr martensitic stainless steels [5].

UNS no.	AISI no. / common name	Fe	Cr	Mn	Si	С	Other
S41000	410	Bal	11.50 13.50	1.00 max	1.00 max	0.15 max	0.040 max P; 0.030 max S
S42000	420	Bal	12.00 14.00	1.00 max	1.00 max	>0.15	0.040 max P; 0.030 max S
S44004	440C	Bal	16.00 18.00	1.00 max	1.00 max	0.95 1.20	0.75 max Mo; 0.040 max P; 0.030 max S

Table 1.1.2. Compositions (wt%) of several heats of Fe-Cr martensitic stainless steels used to study hydrogen effects on mechanical properties.

Heat	Alloy	Fe	Cr	Mn	Si	C	Other	Ref.
W69-410	410	Bal	12.26	0.71	0.60	0.145	0.016 P; 0.007 S; 0.40 Ni; 0.08 Mo; 0.11 Cu; 0.02 Al	[3]
W69-440C	440C	Bal	17.33	0.48	0.33	0.96	0.013 P; 0.024 S; 0.36 Ni; 0.48 Mo	[3]

Material	Thermal precharging	Test environment	Strain rate (s <sup>-1</sup> )	S <sub>y</sub> (MPa)	S <sub>u</sub> (MPa)	El <sub>u</sub> (%)	El <sub>t</sub> (%)	RA (%)	Ref.
410 (heat W69-410)	None	air	0.67	1324	1524		15	60	[3, 6]
	None	69 MPa H <sub>2</sub>	$x10^{-3}$	_	1144	_	1.3	12	
440C (heat W69-440C)	None	air	0.67	1627	2075	_	3.5	3.1	[3, 6]
	None	69 MPa H <sub>2</sub>	$x10^{-3}$	_	820	_	_	0	
	None	air		377	620		7.1		
440C	(1)	air		377	575	_	4.6	_	[2]
	None	air, 200 K	_	406	670		7.7		[2]
	(1)	air. 200 K		450	570		4.2		

Table 3.1.1.1. Smooth tensile properties of martensitic stainless steels at room temperature; measured with internal hydrogen or in external hydrogen gas.

Table 3.1.2.1. Notched tensile properties of martensitic stainless steels at room temperature; measured in external hydrogen gas.

Material	Specimen	Thermal precharging	Test environment	Displ. rate (mm/s)	S <sub>y</sub> † (MPa)	σ <sub>s</sub> (MPa)	RA (%)	Ref.
410	(a)	None	air	~0.35	1324	2730	1.4	[3, 6]
(heat W69-410)	(a)	None	69 MPa H <sub>2</sub>	$x10^{-3}$	_	565	0.6	[5, 0]
440C	(a)	None	air	~0.35	1627	1027	0.6	[2 6]
(heat W69-440C)	(a)	None	69 MPa H <sub>2</sub>	$x10^{-3}$	_	510	0	[3, 6]

<sup>†</sup> yield strength of smooth tensile specimen

<sup>(1) 69</sup> MPa deuterium, 620 K, 500 h (gauge diameter ~ 5 mm)

<sup>(</sup>a) V-notched specimen:  $60^{\circ}$  included angle; minimum diameter = 3.81 mm; maximum diameter = 7.77 mm; notch root radius = 0.024 mm. Stress concentration factor  $(K_t) = 8.4$ .